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(54) **Absorbent structure suitable for use in a sanitary absorbent article**

(57) A sanitary absorbent article, having a fluid-permeable cover layer intended for placement against a body of a wearer when the article is in use by the wearer; a liquid-impervious barrier layer intended to face away from the body of the wearer when the article is in use by the wearer; and an absorbent structure intermediate the cover layer and the barrier layer. The absorbent structure includes a first absorbent layer, the first absorbent layer having a density of between about 0.04 g/cm³ and about 0.09 g/cm³, the first absorbent

layer having superabsorbent particles incorporated therein in an amount no greater than about 15% on a weight per weight basis; and a second absorbent layer having a density of between about 0.25 g/cm³ and about 0.5 g/cm³, the second absorbent layer having superabsorbent particles incorporated therein in an amount no less than about 30% on a weight per weight basis.

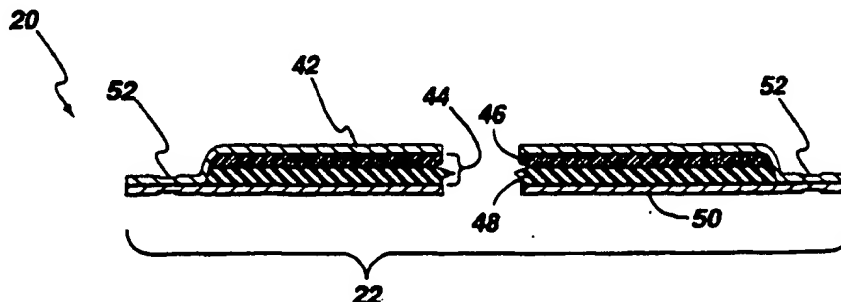


Fig. 4

Description

FIELD OF THE INVENTION

[0001] The present invention relates to sanitary absorbent articles such as feminine sanitary napkins, incontinence pads, infant diapers and the like.

BACKGROUND OF THE INVENTION

[0002] Sanitary absorbent articles generally are large-scale commercially-manufactured articles used to absorb and retain a variety of bodily exudates. Such articles are convenient in that they are often economical yet disposable; they include sanitary napkins, infant diapers, adult incontinence pads and the like.

[0003] Conventional sanitary absorbent articles generally comprise several different layers of material joined together to form a laminate. Each of these layers is referred to as a "component layer" and serves a specific function within the article. Each layer is thus usually fabricated from a material different than that of the others, and has different physical properties and characteristics.

[0004] The uppermost layer of material, i.e. that which faces the body of the wearer of the article is conventionally termed the "cover layer" or "top sheet". As the layer of the article which comes into physical contact with the human body, the cover layer must be relatively soft to the touch so as to avoid discomfort and prevent abrasions to human tissue during the time which the article is worn. The cover layer must be fluid permeable so as to permit the ingress of the bodily exudate into the article to be absorbed and retained. At the same time however, it should remain dry to prevent moisture from accumulating against the skin of the wearer that could cause irritations. In order to meet these desired characteristics, conventional cover layers are manufactured from a non-woven hydrophobic material or a synthetic plastic material having a large number of relatively small apertures per unit surface area.

[0005] Underlying the cover layer is a layer conventionally termed the "absorbent structure", although it is also known by many other names. The purpose of the absorbent structure is to actually absorb and retain bodily exudate deposited on the article. It is extremely desirable that the absorbent structure accomplish these tasks relatively rapidly and permanently. In this respect, the rate at which the exudate is taken up ("the fluid acquisition rate") by the absorbent structure must be such so that it can acquire all of the exudate deposited on the article. Further, the absorbent structure must retain the exudate so absorbed to prevent it from exiting the article. Failure in either sense would mean that fluid has failed to be completely contained by the article, and has soiled the undergarment or garment of the wearer (depending of the type of article and where it is being worn). This is an extremely undesirable situation.

[0006] In order to accomplish these tasks, conventional absorbent structures are typically of a laminate structure themselves. They commonly comprise a first absorbent layer underlying the cover layer, and a second absorbent layer underlying the first absorbent layer. Preferably, the first absorbent layer has a relatively more dense structure than the cover layer and a relatively less dense structure than the second absorbent layer to absorb fluid quickly from the cover layer and distribute it quickly to the second absorbent layer. The first absorbent layer may commonly be called a "fluid acquisition layer" or a "transfer layer". The second absorbent layer may commonly be called an "absorbent core". Each of these layers serves a different purpose. In order to understand the purpose and function of these layers, reference must be had to absorbent structures that existed before the creation of these types of absorbent structures.

[0007] Prior to the dual absorbent layer structure of absorbent structures, a common design of these structures was a single absorbent layer. Typically this layer comprised cellulosic fibers (e.g. wood pulp), and in order to absorb the relatively large quantities of exudate that the article was intended to absorb, and still remain of a manageable size, the absorbent layer was relatively dense. While this density imparted to the absorbent layer the required exudate absorbent capacity, it created several drawbacks. One drawback was the exudate acquisition rate of such a structure. In many instances this rate was too slow to absorb immediately all of the exudate deposited on the article. Exudate not immediately absorbed would pool on the cover layer and flow off the article.

[0008] A second, and related, drawback was local saturation. Sanitary absorbent articles are intended to absorb bodily exudate emanating from a single source fixed in space relative to the article. Thus, the exudate to be absorbed is constantly deposited on the article in the same place. Owing to its density, the rate at which exudate absorbed by the absorbent layer is wicked through its structure to points other than the exudate's initial point of deposit on the article, is slow. Hence, in some instances the initial point of deposit becomes saturated and the rate at which exudate is removed away from this point by wicking is not as fast as the rate at which fresh exudate is being deposited on the article. Again, this would cause the exudate to pool on the cover layer and flow off the article.

[0009] A first absorbent layer was added to these absorbent layers to attempt to remedy some of these drawbacks. Such first absorbent layers also comprise cellulosic material, however, they are much less dense. They have very rapid exudate acquisition rates and easily wick exudate throughout their volume. Thus they cooperate with absorbent layers (now termed second absorbent layers) in the following manner. Exudate to be absorbed by the article is initially deposited on the cover layer of the article and flows therethrough to the

first absorbent layer. The exudate acquisition rate of the first absorbent layer is greater than the exudate deposition rate such that all of the exudate is relatively rapidly absorbed into the first absorbent layer. The exudate is then rapidly spread throughout the volume of the first absorbent layer, which avoids local saturation of the first absorbent layer at any one particular point. The first absorbent layer, however, does not have a large absorbent capacity, and it is not intended that the exudate remain there for any relatively long period of time. It is intended that the exudate migrate through the first absorbent layer to the second absorbent layer therebelow. Because of the presence and function of the first absorbent layer, however, the exudate is effectively presented to the second absorbent layer across a much larger portion of its surface area. Hence, problems of local saturation in the second absorbent layer are minimized or avoided. Further, the first absorbent layer acts to store the exudate and meter it to the second absorbent layer at a rate at which the latter can absorb it. Hence, the problem of the slow acquisition rate of the second absorbent layer has also been minimized or avoided.

[0010] While the addition of first absorbent layers to absorbent structures of sanitary absorbent articles did alleviate some of the prior difficulties of such structures, it was not entirely optimal. In order to have the first absorbent layer and second absorbent layer function in the cooperative manner described above, the second absorbent layer must have a greater fluid retention capacity than the first absorbent layer.

[0011] The relatively lower fluid retention capacity of the first absorbent layer, as compared with that of the second absorbent layer, has some undesirable consequences. One particular undesirable consequence is surface moisture. Surface moisture is moisture that accumulates on the surface of the cover layer and is felt by the wearer of the article. (As described above it is undesirable.) Some moisture will always diffuse out of the absorbent structure, but more will diffuse out when the layer underlying the cover layer is a first absorbent layer as opposed to a second absorbent layer, because of the difference in retention power between these structures. It would be desirable if the surface moisture attributable to the first absorbent layer could be reduced.

[0012] Therefore there exists a need in the art for an improved absorbent structure suitable for use in a sanitary absorbent article. Particularly, there exists a need in the art for an improved absorbent structure comprising a first absorbent layer and a second absorbent layer, having a reduced incidence of surface moisture as compared with some conventional designs.

OBJECT AND STATEMENT OF THE INVENTION

[0013] It is therefore an object of the present invention to provide an improved absorbent structure suitable

for use in a sanitary absorbent article, and an article containing such structure.

[0014] The present inventors have realized that the incidence of surface moisture may be decreased in absorbent structures of this type, if superabsorbent material in certain ratios is added to a first absorbent layer and a second absorbent layer having certain densities.

[0015] Thus, as embodied and broadly described herein, the present invention provides a sanitary absorbent article, comprising:

- (A) a fluid-permeable cover layer intended for placement against a body of a wearer when the article is in use by the wearer;
- (B) a liquid-impervious barrier layer intended to face away from the body of the wearer when the article is in use by the wearer;
- (C) an absorbent structure intermediate said cover layer and said barrier layer, said absorbent structure comprising:

(i) a first absorbent layer, said first absorbent layer having a density of between about 0.04 g/cm³ and about 0.09 g/cm³, said first absorbent layer having superabsorbent particles incorporated therein in an amount no greater than about 15% on a weight per weight basis; and

(ii) a second absorbent layer having a density of between about 0.25 g/cm³ and about 0.5 g/cm³ said second absorbent layer having superabsorbent particles incorporated therein in an amount no less than about 30% on a weight per weight basis.

[0016] As described above, the primary purpose of the cover layer of the article is to protect the skin of the wearer of the article from the exudate absorbed and retained by the interior of the article, keeping the skin of the wearer dry. It must however, allow the exudate to be absorbed to pass through it. In the context of the present invention, any conventional cover layer, constructed by conventional means, will suffice.

[0017] The first absorbent layer of the present invention may be constructed of any conventional material that is suitable for forming a transfer layer or fluid acquisition layer (or the like) of a sanitary absorbent article once the absorbent structure is incorporated into the article. Thus, for instance, the first absorbent layer may, preferably comprise cellulosic material. In this context, the term "cellulosic material" should be understood as encompassing both cellulosic fibers and cellulosic particulate. Non-limiting examples of cellulosic material thus include: all types of wood fibers, cotton linters, bagasse, flax, jute, straw, bamboo, esparto, grass, sphagnum, etc. Cellulose is the carbohydrate forming the main constituent of plant cell walls, and thus there

are many types of plants that may be used to form cellulosic materials, whether or not such plants are actually used to form such materials at the present time. The first absorbent layer may also comprise synthetic fibers such as polyester, rayon, and flexible foam fibers. It may also comprise combinations of any or all of these.

[0018] As stated above, the first absorbent layer has a density of between about 0.04 g/cm³ and about 0.09 g/cm³. Preferably, the density of the first absorbent layer is between about 0.05 g/cm³ and about 0.08 g/cm³. More preferably, the density of the first absorbent layer is between about 0.06 g/cm³ and about 0.07 g/cm³.

[0019] Incorporated into the first absorbent layer are superabsorbent particles. Superabsorbent particles are materials that are capable of absorbing many times, preferably 10, more preferably 15, and still more preferably over 15, their weight in exudate. It should be noted that, in the context of the present invention, there is no restriction that the superabsorbent particles, actually be particulate. This expression is intended to cover superabsorbent fibers, and other superabsorbent materials, whatever their form and shape. These superabsorbent particles generally fall into three classes, namely starch graft copolymers, crosslinked carboxymethylcellulose derivatives and modified hydrophilic polyacrylates. Examples of such absorbent polymers are hydrolized starch-acrylonitrile copolymer graft copolymer, a neutralized starch-acrylic acid graft copolymer, a saponified acrylic acid ester-vinyl acetate copolymer, a hydrolyzed acrylonitrile copolymer or acrylamide copolymer, a modified cross-linked polyvinyl alcohol, a neutralized self-crosslinking polyacrylic acid, a crosslinked polyacrylate salt, carboxylated cellulose, and a neutralized crosslinked isobutylene-maleic anhydride copolymer. The most preferred superabsorbent particle is a crosslinked polyacrylate salt.

[0020] As stated above, the superabsorbent particles are incorporated into the first absorbent layer in an amount no greater than about 15% on a weight per weight basis. Preferably, they are incorporated in an amount between about 5% and about 12% on a weight per weight basis. More preferably, they are incorporated in an amount between about 5% and about 10%. In the present context 15% superabsorbent on "a weight per weight basis" is meant to 0.15 grams of superabsorbent particles per 1 gram of all components comprising the first absorbent layer.

[0021] A first absorbent layer of the present invention may be constructed according to conventional techniques, e.g. by air-laying a mixture of wood pulp fibers and superabsorbent material. All such conventional techniques are within the scope of the present invention.

[0022] The second absorbent layer of the present invention may be constructed of any conventional material that is suitable for that purpose. Thus, for instance, the second absorbent layer preferably comprises cellu-

losic material. The second absorbent layer may also comprise synthetic fibres such as polyester, rayon, polyolefin and flexible foam fibers. It may also comprise combinations of any or all of these. The second absorbent layer may comprise the same material or combination of materials as the first absorbent layer (in terms of composition and dimension), but it need not. The two may actually be different zones of a single integrated physical structure.

[0023] As further stated above, the second absorbent layer has a density of between about 0.25 g/cm³ and about 0.5 g/cm³. Preferably, the density of said second absorbent layer is between about 0.3 g/cm³ and about 0.4 g/cm³.

[0024] Incorporated into said second absorbent layer are superabsorbent particles. The superabsorbent particles incorporated into the second absorbent layer may be the same particles as incorporated into the first absorbent layer (in terms of composition and dimension), but they need not. The most preferred superabsorbent particles incorporated into the second absorbent layer is a crosslinked polyacrylate salt.

[0025] Preferably, the superabsorbent particles are incorporated into said second absorbent layer in an amount between about 20% and about 55% on a weight per weight basis. More preferably, the superabsorbent particles are incorporated into said second absorbent layer in an amount between 30% and 45% on a weight per weight basis. Most preferably, the superabsorbent particles are incorporated into said second absorbent layer in an amount between 35% and 45% on a weight per weight basis. In the present context 45% superabsorbent on "a weight per weight basis" is meant to 0.45 grams of superabsorbent particles per 1 gram of all components comprising the second absorbent layer.

[0026] A second absorbent layer of the present invention may be constructed according to conventional techniques, e.g. by air-laying a mixture of wood pulp fibers and superabsorbent material. All such conventional techniques are within the scope of the present invention. A preferred second absorbent layer is as described in United States Patent 5,866,242 to Tan *et al.*, which is herein incorporated by reference in its entirety.

[0027] Underneath the absorbent structure is the barrier layer. The primary purpose of the barrier layer is to prevent exudate absorbed within the article from egressing the article on the opposite surface from which it was absorbed. The barrier layer is thus impervious to liquid but could be made pervious to gases to provide breathability. All conventional barrier layers are within the scope of the present invention.

[0028] Preferably, the cover layer and the barrier layer are joined to one another around the periphery of the article to form an envelope or casing enclosing the absorbent structure and forming a structurally integral article. It is preferred that this envelope surround, and thus contain, the absorbent structure within it. Other conventional methods of adhering or uniting the various

components of the article together, such as adhesive between the components, are all also within the scope of the present invention.

[0029] Preferably, the article is a sanitary napkin, pantliner, or an incontinence pad.

[0030] Sanitary absorbent articles constructed in accordance with the present invention have several advantages. Most advantageously, they have a reduced incidence of surface moisture, translating to a "drier feeling" against the skin of the wearer. In addition, these articles do not experience a significant amount of "gel-blocking". Gel-blocking is a phenomenon with which those skilled in the art are familiar. When superabsorbent material absorbs a large quantity of fluid it swells. Gel-blocking occurs when superabsorbent material across an expanse of the article absorbs a significant amount of fluid and swells together forming a weight which is difficult or impossible for additional exudate to penetrate. Thus, when gel-blocking occurs, the swelled superabsorbent seals off the absorbent material below it, effectively rendering it much less useful. The combination first absorbent layer / second absorbent layer of the present invention have the additional advantage that gel-blocking is minimized.

[0031] Other aspects and features of the present invention will become apparent in those ordinarily skilled in the art upon review of the following description of specific embodiments of the invention in conjunction with the accompanying drawings. In the drawings, preferred embodiments of the invention are illustrated by way of example. It is to be expressly understood that the description and drawings are only for purposes of illustration and as aid to understanding, and are not intended to be a definition of the limits of the invention.

DESCRIPTION OF THE DRAWINGS

[0032]

Figure 1 is a top elevational view of a sanitary napkin in accordance with the present invention, the cover layer of the sanitary napkin being partly removed to show the absorbent system;

Figure 2 is a perspective view of the sanitary napkin of Figure 1, depicted in a position attained when the sanitary napkin is placed in the undergarment of a wearer;

Figure 3 is a bottom plan view of the sanitary napkin shown in Figure 1;

Figure 4 is a cross-sectional view taken along the longitudinal centerline of the sanitary napkin shown in Figure 3;

Figure 5 is a schematic illustration of means for air-laying absorbent material for making an example of

a second absorbent layer of the sanitary napkin according to the invention, using four air-laying heads followed by means for compacting the air-laid material;

Figure 6a shows a three stratum embodiment of a second absorbent layer that can be used in the sanitary napkin in accordance with the invention; and

Figure 6b shows a four stratum embodiment of a second absorbent layer that can be used in the sanitary napkin in accordance with the invention.

[0033] In the drawings, preferred embodiments of the invention are illustrated by way of example. It is to be expressly understood that the description and drawings are only for purposes of illustration and as aid to understanding, and are not intended to be a definition of the limits of the invention.

DETAILED DESCRIPTION OF PREFERRED EMBODIMENTS

[0034] Referring to Figures 1 and 2, there is shown an embodiment of the present invention, a feminine sanitary napkin 20.

[0035] The sanitary napkin 20 has a main body 22 with a first transverse side 26 defining a front portion thereof and a second transverse side 28 defining a rear portion thereof. Each of these sides is arcuate. The main body also has two longitudinal sides, namely a longitudinal side 30 and a longitudinal side 32. The sanitary napkin 20 has a thickness not exceeding about 5 mm. Preferably, the thickness is less than 3.5 mm, more preferably less than 3 mm, and most preferably, it is of about 2.8 mm.

[0036] The sanitary napkin 20 has a longitudinal centerline 34 that is an imaginary line bisecting the sanitary napkin 20 in two identical halves.

[0037] Projecting laterally outward from each of the longitudinal sides 30, 32 is a flap 38, 40 (respectively). The flaps 38, 40 are in the shape of an isosceles trapezoid with the top adjoining the longitudinal side and the base at the distal end. The main body 22 also has an imaginary transverse centerline 36 perpendicular to the longitudinal centerline 34 and simultaneously bisecting the flaps 38, 40.

[0038] As depicted in Figure 4, the main body 22 is of a laminate construction and preferably comprises a fluid-permeable cover layer 42, an absorbent system 44, and a fluid-impervious barrier layer 50. The absorbent system has preferably two components, namely a first absorbent layer 46 (commonly known as "transfer layer") and a second absorbent layer 48 (commonly known as "absorbent core"). Each of these layers is described hereinbelow.

Main Body-Cover Layer

[0039] The cover layer 42 may be a relatively low density, bulky, high-loft non-woven web material. The cover layer 42 may be composed of only one type of fiber, such as polyester or polypropylene or it may be composed of bi-component or conjugate fibers having a low melting point component and a high melting point component. The fibers may be selected from a variety of natural and synthetic materials such as nylon, polyester, rayon (in combination with other fibers), cotton, acrylic fiber and the like and combinations thereof. An example is the non-woven cover layer of sanitary napkins sold by Johnson & Johnson Inc. of Montreal, Canada under the trademark Stayfree Ultra-Thin Cottony Dry Cover.

[0040] Bi-component fibers may be made up of a polyester core and a polyethylene sheath. The use of appropriate bi-component materials results in a fusible non-woven fabric. Examples of such fusible fabrics are described in U.S. Patent 4,555,446 issued November 50, 1965 to Mays. Using a fusible fabric increases the ease with which the cover layer may be mounted to the adjacent first absorbent layer and/or to the barrier layer.

[0041] The cover layer 42 preferably has a relatively high degree of wettability, although the individual fibers comprising the cover may not be particularly hydrophilic. The cover material should also contain a great number of relatively large pores. This is because the cover layer 42 is intended to take-up body fluid rapidly and transport it away from the body and the point of deposition. Advantageously, the fibers which make up the cover layer 42 should not lose their physical properties when they are wetted, in other words they should not collapse or lose their resiliency when subjected to water or body fluid. The cover layer 42 may be treated to allow fluid to pass through it readily. The cover layer 42 also functions to transfer the fluid quickly to the other layers of the absorbent system 44. Thus, the cover layer 42 is advantageously wettable, hydrophilic and porous. When composed of synthetic hydrophobic fibers such as polyester or bi-component fibers, the cover layer 42 may be treated with a surfactant to impart the desired degree of wettability.

[0042] Alternatively, the cover layer 42 can also be made of polymer film having large pores. Because of such high porosity, the film accomplishes the function of quickly transferring body fluid to the inner layers of the absorbent system. Apertured co-extruded films such described in U.S. Patent 4,690,679 and available on sanitary napkins sold by Johnson & Johnson Inc. of Montreal, Canada could be useful as cover layers in the present invention.

[0043] The cover layer 42 may be embossed to the remainder of the absorbent system 44 in order to aid in promoting fluid transport by fusing the cover to the next layer. Such fusion may be effected locally, at a plurality of sites or over the entire contact surface of cover layer

42 with absorbent system 44. Alternatively, the cover layer 42 may be attached to the absorbent system 44 by other means such as by adhesive.

Main Body - Absorbent System -First Absorbent Layer

[0044] Adjacent to the cover layer 42 on its inner side and bonded to the cover layer 42 is a first absorbent layer 46 that forms part of the absorbent system 44.

The first absorbent layer 46 provides the means of receiving body fluid from the cover layer 42 and holding it until an underlying second absorbent layer has an opportunity to absorb the fluid.

[0045] In one embodiment, the first absorbent layer 46, is a blend or mixture of cellulosic fibres and superabsorbent disposed in and amongst fibers of that pulp.

[0046] In a specific example, the first absorbent layer 46 is a material containing from about 75 weight percent to about 95 weight percent cellulosic fibers; and from about 5 weight percent to about 15 weight percent SAP (superabsorbent polymers). The material has a water content of less than about 10 weight percent. As used herein, the phrase "weight percent" means weight of substance per weight of final material. By way of example, 10 weight percent SAP means 10 g/m² SAP per 100g/m² basis weight of the material.

[0047] Cellulosic fibers that can be used in the first absorbent layer 46 are well known in the art and include wood pulp, cotton, flax and peat moss. Wood pulp is preferred. Pulp can be obtained from mechanical or chemimechanical, sulfite, kraft, pulping reject materials, organic solvent pulps, etc. Both softwood and hardwood species are useful. Softwood pulps are preferred. It is not necessary to treat cellulosic fibers with chemical debonding agents, cross-linking agents and the like for use in the present material.

[0048] The first absorbent layer 46 can contain any superabsorbent particle (SAP), which SAPs are well known in the art. For the purposes of the present invention, the term "superabsorbent particle" (or "SAP") refers to materials which are capable of absorbing and retaining at least about 10 times their weight in body fluids, preferably under a 0.5 psi pressure. The superabsorbent particles of the invention may be inorganic or organic crosslinked hydrophilic polymers, such as polyvinyl alcohols, polyethylene oxides, crosslinked starches, guar gum, xanthan gum, and the like. The particles may be in the form of a powder, grains, granules, or fibers. Preferred superabsorbent polymer particles for use in the first absorbent layer are crosslinked polyacrylates that have a slow rate of absorption than those of the second absorbent layer 48 (described below), such as the product offered by Chemdal International, Inc. of Palatine, Illinois, under the designation of 2100A*.

[0049] The first absorbent layer 46 is manufactured in a similar manner to that described below in relation to the second absorbent layer 48.

[0050] An example of a suitable first absorbent layer is a through air bonded pulp sold by BUCKEYE of Memphis Tennessee under the designation VIZORB 3008 to which SAP may be incorporated.

Main Body - Absorbent System-Second Absorbent Layer

[0051] Immediately adjacent to and bonded to the first absorbent layer 46 is the second absorbent layer 48.

[0052] In one embodiment, the first absorbent layer 46 has a central width that is at least about the same as the central width of the second absorbent layer 48. In a specific embodiment, this central width is greater than about 60 mm. In another embodiment, the first absorbent layer 46 has a central width that exceeds the central width of the second absorbent layer 48. The term "central width" refers to a specific area of a layer, such as an absorbent layer determinable as follows. A reference point on the sample layer that is disposed beneath the center of the vaginal orifice, when worn, is located. A plane parallel to the transverse centerline 36 and 3.75 centimeters forward from the reference point in the direction of the wearer's mons pubis is located. Another plane parallel to the lateral centerline 36 and 5.0 centimeters rearward from the reference point in the direction of the wearer's buttocks is also located. The greatest flat-out, uncompressed, unmanipulated, lateral width of the sample layer between the two planes is the absorbent width of the sample layer.

[0053] The central width of the absorbent system, when the absorbent system includes a plurality of absorbent layers is the central width of the layer of the absorbent system that has the largest central width. In a specific example, the central width of the absorbent system exceeds 60 mm.

[0054] In one embodiment, the second absorbent layer 48 is a blend or mixture of cellulosic fibers and superabsorbent.

[0055] In a specific example, the second absorbent layer 48 is a material containing from about 40 weight percent to about 65 weight percent cellulosic fibers; and from about 30 weight percent to about 60 weight percent SAP (superabsorbent polymers). The material has a water content of less than about 10 weight percent. As used herein, the phrase "weight percent" means weight of substance per weight of final material. By way of example, 10 weight percent SAP means 10 g/m² SAP per 100g/m² basis weight of the material.

[0056] Cellulosic fibers that can be used in the second absorbent layer 48 are well known in the art and include wood pulp, cotton, flax and peat moss. Wood pulp is preferred. Pulp can be obtained from mechanical or chemical-mechanical, sulfite, kraft, pulping reject materials, organic solvent pulps, etc. Both softwood and hardwood species are useful. Softwood pulps are preferred. It is not necessary to treat cellulosic fibers with

chemical debonding agents, cross-linking agents and the like for use in the present material.

[0057] The second absorbent layer 48 can contain any SAP well known in the art. Preferred superabsorbent particles for use in the second absorbent layer 48 of the present invention are crosslinked polyacrylates that have a faster rate of absorption than those of the superabsorbent particles used in the first absorbent layer 46, such as the product offered by Sumitomo Seika Chemicals Co., Ltd. Of Osaka, Japan, under the designation of SA60N Type II*.

[0058] The second absorbent layer 48 can be manufactured by using airlaying means well known in the art (See Figure 5). In accordance with Figure 5, cellulosic fibers (e.g., pulp) are processed using a hammer mill to individualize the fibers. The individualized fibers are blended with SAP granules in a blending system 1 and pneumatically conveyed into a series of forming heads 2. The blending and distribution of fibers and SAP granules can be controlled separately for each forming head. Controlled air circulation and winged agitators in each chamber produce uniform mixture and distribution of pulp and SAP. The SAP can be thoroughly and homogeneously blended throughout the material or contained only in specific strata by distributing it to selected forming heads. Fibers (and SAP) from each forming chamber are deposited by vacuum onto a forming wire 3 thus forming a layered absorbent web. The web is subsequently compressed using calenders 4 to achieve desirable density. The densified web is wound into a roll 5 using conventional winding equipment. The forming wire 3 can be covered with tissue paper to reduce the loss of material. The tissue paper layer can be removed prior to calendering or incorporated into the formed material. In a possible variant, the first absorbent layer 46 can be formed integrally with the second absorbent layer 48 to provide a unitized absorbent system 44. This can be achieved by providing the apparatus depicted in Figure 5 with an additional forming head (not shown in the drawings) to deposit on the second absorbent layer 48, by air laying and prior to calendering, a layer of material to form the first absorbent layer 46.

[0059] The second absorbent layer 48 of the present invention is of high density and in a specific example has a density of greater than about 0.25 g/cc. Specifically, the second absorbent layer 48 may have a density in the range of from about 0.30 g/cc to about 0.50 g/cc. More specifically, the density is from about 0.30 g/cc to about 0.45 g/cc and, even more specifically from about 0.30 g/cc to about 0.40 g/cc.

[0060] Air-laid absorbents are typically produced with a low density. To achieve higher density levels, such as the examples of the second absorbent layer 48 given above, the air-laid material is compacted using calenders as shown in Figure 5. Compaction is accomplished using means well known in the art. Typically such compaction is carried out at a temperature of about 100 degrees C and a load of about 130 Newtons

per millimeter. The upper compaction roll is typically made of steel while the lower compaction roll is a flexroll having a hardness of about 85 SH D. It is preferred that both the upper and lower compaction rolls be smooth, although the upper roll can be engraved.

[0061] In one embodiment the second absorbent layer 48 has a ratio of Gurley stiffness, measured in milligrams (mg) to density, measured in grams per cubic centimeter (g/cc), of less than about 3700. In a specific example, that ratio of Gurley stiffness to density is less than about 3200 and, more specifically, less than about 3000.

[0062] Gurley stiffness is one of many indices of softness. Gurley stiffness measures the bendability or flexibility of absorbent materials. The lower the Gurley stiffness value, the more flexible the material. The Gurley stiffness values are measured using a Gurley Stiffness Tester (Model No. 4171E), manufactured by Gurley Precision Instruments of Troy, N.Y. The instrument measures the externally applied moment required to produce a given deflection of a test strip of specific dimensions fixed at one end and having a concentrated load applied to the other end. The results are obtained in "Gurley Stiffness" values in units of milligrams.

[0063] The second absorbent layer 48 is strong despite its relative softness. Pad integrity is a well-known measurement of absorbent material strength. In a specific embodiment the second absorbent layer 48 demonstrates strength (high pad integrity) over a wide range of densities. In a specific example the second absorbent layer 48 has a pad integrity, measured in Newtons (N), to density (g/cc) ratio of greater than about 25.0. In a more specific example, that ratio is greater than about 30.0 and, could even be greater than about 35.0. The pad integrity is a test performed on an Instron Universal Testing Machine. Essentially, the test measures the load required to pierce through the test sample, as described in the PFI Method of 1981. A test sample having dimensions of 50 mm by 50 mm is clamped on the Instron with a suitable fastening device. A 20 mm diameter piston traveling at the rate of 50 mm/mm punctures the stationary sample. The force required to puncture the sample is measured in Newtons (N).

[0064] The second absorbent layer 48 can be prepared over a wide range of basis weights. The second absorbent layer 48 can have a basis weight in the range of from about 100 g/m² to about 700 g/m². In a specific example, the basis weight ranges from about 150 g/m² to about 350 g/m². Preferably the basis weight ranges from about 200 g/m² to about 300 g/m² and, more preferably, to about 250 g/m².

[0065] The second absorbent layer 48 can be formed as three or four lamina or strata. Those strata include a bottom layer, one or two middle layers and a top layer. Specific examples of three and four layer material are set forth below. The SAP can be included in any or all of the layers. The concentration (weight per-

cent) of SAP in each layer can vary as can the nature of the particular SAP.

[0066] An interesting characteristic of the second absorbent layer 48 is its ability to retain SAP when subjected to mechanical stress. The second absorbent layer 48 retained over 85 percent by weight of its SAP content when subjected to 10 minutes of rigorous shaking. Specifically, a material of this invention retains over 90 percent, more specifically over 95 percent and, even more specifically over 99 percent of its SAP under these mechanical stresses. The percent of SAP retained was determined by shaking the material in a Ro-Tap Sieve Shaker manufactured by W. S. Tyler Co., Cleveland Ohio. More specifically the sample is placed in a 28-mesh (Tyler series) sieve. Additional sieves of 35-mesh and 150-mesh were attached to the first sieve forming a column of increasingly fine sieves. The column of sieves was capped on either end to prevent the loss of fiber and/or SAP. The sieve column was placed in the shaker and agitated for 10 minutes. The amount of SAP granules shaken loose from the sample, "free SAP", was determined by combining the residue contained in each of the sieves and separating the cellulosic fiber from the SAP.

[0067] Even where prepared as from multiple layers, the final thickness of the formed second absorbent layer 48 is low. The thickness can vary from about 0.5 mm to about 2.5 mm. In a specific example, the thickness is from about 1.0 mm to about 2.0 mm and, even more specifically from about 1.25 mm to about 1.75 mm.

[0068] One embodiment of the second absorbent layer 48 particularly well suited for use in the sanitary napkin 20 is depicted in Figure 6. Such second absorbent layer 48 has a basis weight of from about 200 g/m² to about 350 g/m² and a density between about 0.3 g/cc and 0.5 g/cc. In a specific example, the density is from about 0.3 g/cc to about 0.45 g/cc and, more specifically about 0.03-0.04 g/cc.

[0069] The second absorbent layer 48 depicted in Figure 6 is air-laid as three strata: a bottom layer of pulp (without superabsorbent) with a basis weight of about 25 g/m²; a middle layer with a basis weight of about 150 g/m² and which contains from about 10 to about 30 g/m² superabsorbent and from about 120 g/m² to about 140 g/m² pulp; and a top layer of pulp (without superabsorbent) with a basis weight of about 25 g/m². Relative to the total basis weight of the second absorbent layer 48, the level of superabsorbent ranges from about 5 to about 15 weight percent (g/m² of superabsorbent per g/m² material). In a specific example, the level of superabsorbent is from about 7.5 weight percent to about 12.5 weight percent of the material. More specifically, the material contains about 10 weight percent of superabsorbent. Thus, the middle layer of the material could contain from about 15 g/m² to about 25 g/m² superabsorbent and from about 125 g/m² to about 135 g/m² pulp and, more specifically about 20 g/m² superabsorb-

ent and about 130 g/m² pulp. The middle layer containing pulp and superabsorbent can be laid down as a homogeneous blend or as a heterogeneous blend wherein the level of superabsorbent varies with proximity to the bottom layer.

[0070] In another embodiment, the second absorbent layer 48 is air-laid as four strata. In this embodiment, the middle layer referred to above is replaced with two middle layers: a first middle layer adjacent the top layer and a second middle layer adjacent the bottom layer. Each of the first and second middle layers independently comprises from about 10 to about 30 g/m² superabsorbent and from about 40 g/m² to about 65 g/m² pulp. When it is desired to keep absorbed fluid away from the cover layer 42 the amount of superabsorbent in the first and second middle layers is adjusted such that there is a higher level of superabsorbent in the second middle layer. The superabsorbents in the first and second middle layers can be the same or different.

[0071] In one embodiment, the cellulosic fiber for use in the second absorbent layer 48 is wood pulp. There are certain characteristics of wood pulp that make it particularly suitable for use. Cellulose in most wood pulps has a crystalline form known as Cellulose I which can be converted to a form known as Cellulose II. In the second absorbent layer 48, wood pulp with a substantial portion of the cellulose as Cellulose II could be used. Similarly, pulps having an increased fiber curl value are advantageous. Finally, pulps having reduced levels of hemicellulose are preferred. Means for treating pulps so as to optimize these characteristics are well known in the art. By way of example, treating wood pulp with liquid ammonia is known to convert cellulose to the Cellulose II structure and to increase the fiber curl value. Flash drying is known to increase the fiber curl value of pulp. Cold caustic treatment of pulp decreases hemicellulose content, increases fiber curl and converts cellulose to the Cellulose II form. Thus it could be advantageous that the cellulosic fibers used to produce the material of this invention contain at least a portion of cold caustic treated pulp.

[0072] A description of the cold caustic extraction process can be found in U.S. patent application Ser. No. 08/370,571, filed on Jan. 18, 1995, pending which application is a continuation-in-part application of U.S. patent application Ser. No. 08/184,377, now abandoned filed on Jan. 21, 1994. The disclosures of both of these applications are incorporated in their entirety herein by reference.

[0073] Briefly, a caustic treatment is typically carried out at a temperature less than about 60 degree C., but preferably at a temperature less than 50 degree C., and more preferably at a temperature between about 10 degree C. to 40 degree C. A preferred alkali metal salt solution is a sodium hydroxide solution newly made up or as a solution by-product in a pulp or paper mill operation, e.g., hemicaustic white liquor, oxidized white liquor and the like. Other alkali metal salts such as

ammonium hydroxide and potassium hydroxide and the like can be employed. However, from a cost standpoint, the preferable salt is sodium hydroxide. The concentration of alkali metal salts is typically in a range from about 2 to about 25 weight percent of the solution, and preferably from about 6 to about 18 weight percent. Pulps for high rate, fast absorbing applications are preferably treated with alkali metal salt concentrations from about 10 to about 18 weight percent.

[0074] For further details on the structure and the method of construction of the second absorbent layer 48 the reader is invited to refer to the US patent 5,866,242 granted on February 2, 1999 to Tan et al. The contents of this document are hereby incorporated by reference.

Main Body-Barrier Layer

[0075] Underlying the absorbent system 44 is a barrier layer 50 comprising liquid-impervious film material so as to prevent liquid that is entrapped in the absorbent system 44 from egressing the sanitary napkin and staining the wearer's undergarment. The barrier layer 50 is made of polymeric film.

[0076] The cover layer 42 and the barrier layer 50 are joined along their marginal portions so as to form an enclosure or flange seal that maintains the absorbent system 44 captive. The joint may be made by means of adhesives, heat-bonding, ultrasonic bonding, radio frequency sealing, mechanical crimping, and the like and combinations thereof. The peripheral seal line is shown in Figure 1 by the reference numeral 52.

Flaps

[0077] The flaps 38 and 40 are preferably made as integral extensions of the cover layer 42 and the barrier layer 50. These integral extensions are joined to one another along their marginal seal portions by adhesives, heat-bonding, ultrasonic bonding, radio frequency sealing, mechanical crimping, and the like and combinations thereof. Most preferably, such joining is made at the same time the cover layer 42 and the barrier layer 50 are bonded to one another to enclose the absorbent system 44. Alternatively, the flaps may include absorbent material between the cover layer and the barrier layer extensions. Such absorbent material may be an extension of the first absorbent layer 46, the second absorbent layer 48 or both. The flaps are optional and may have another suitable shape than the one shown.

Adhesive system

[0078] Referring to Figures 2 and 3, in order to enhance the stability of the sanitary napkin, the garment facing surface of the barrier layer is provided with positioning adhesive material 58, typically hot-melt adhesive material capable of establishing a temporary bond with

the undergarment material. A suitable material is the composition designated HL-1491 XZP commercially available from H.B. Fuller Canada, Toronto, Ontario, Canada. The positioning adhesive 58 may be applied to the garment-facing surface of the barrier layer 50 in various patterns, including complete adhesive coverage, parallel longitudinal lines, a line of adhesive following the perimeter of the structure, transverse lines of adhesive or the like.

[0079] Standard release paper 82 (shown only in Figure 3) covers the positioning adhesive 58 before the napkin is used to prevent the unwanted adherence of the napkin to itself or foreign objects. The release paper is of convention construction (e.g. silicone coated wet-laid Kraft wood pulp) and suitable papers are available from Tekkote Corporation (Leonia, New Jersey, USA), and bear the designation FRASER 30#/61629.

Method of manufacture

[0080] The above-described embodiment of the sanitary napkin 20 is fabricated in a conventional manner in accordance with conventional techniques. Specifically, a laminate structure, sometimes referred to in the art as a web, is created. This laminate structure comprises an expanse of the materials from which the napkin will be created. I.e. the laminate structure comprises the following layers of material in a top-to-bottom order: an expanse of cover layer material; an expanse of first absorbent layer material; an expanse of second absorbent layer material (manufactured as described above); and finally an expanse of barrier layer. Some of the materials are necessarily not continuous within the laminate structure, and where such is the case, they are positioned precisely, one with respect to another, in the relationship they will occupy in the final products. The cover layer material and the barrier layer material are then bonded together by applying pressure in the appropriate positions, and what will become the peripheral seal is created. (The seal may also be made by means of heat-bonding, ultrasonic bonding, radio frequency sealing, mechanical crimping, and the like and combinations thereof.) The sealed structure is then severed by conventional means (i.e. die-cutting, fluid-jet cutting, or by laser) from the web to create a discrete article.

[0081] The positioning adhesive material is then applied to the barrier layer in the appropriate positions, and release paper is applied to cover the positioning adhesive. Alternatively, the positioning adhesive, or the positioning adhesive and the release paper may be applied to the web before the individual articles are severed therefrom.

[0082] As indicated earlier, the sanitary napkin 20 has a thickness of about 5 mm or less. The apparatus required to measure the thickness of the sanitary napkin is a footed dial (thickness) gauge with stand, available from Ames, with 2" diameter foot and a readout

accurate to 0.001". A digital type apparatus is preferred.

[0083] If the sanitary napkin sample is individually folded and wrapped, the sample is unwrapped and carefully flattened by hand. The release paper is removed from the sample and it is repositioned back gently across the positioning adhesive lines so as not to compress the sample, ensuring that the release paper lies flat across the sample. Flaps (if any) are not considered when taking the thickness reading of the sample.

[0084] The foot of the gauge is raised and the sample is placed on the anvil such that the foot of the gauge is approximately centered to the sample (or in the location of interest on the sample of interest). When lowering the foot, care is taken to avoid the foot to "drop" or that undue force is not applied. A load of 0.07 p.s.i.g. is applied to the sample and the read out is allowed to stabilize for approximately 5 seconds. The thickness reading is then taken. The thickness of the release paper covering the positioning adhesive is deducted from the total thickness.

[0085] The sanitary napkin 20 is characterized by excellent absorption properties and at the same time it has a level of flexural resistance sufficient to reduce the incidence of bunching in use. More particularly, the sanitary napkin 20 has a test capacity of more than about 8 g of fluid and a total capacity of more than about 14 g of fluid. The test and total capacities of a sanitary napkin are determined as follows. Any panty adhesive release paper is removed from the napkin to be tested. To determine test capacity, a 4.75 cm by 14.0 cm portion of the sanitary napkin is cut from the portion of the sanitary napkin which would be centered under the vaginal orifice when the sanitary napkin is worn. Total capacity is determined using the entire napkin minus any release paper. The article is weighed to the nearest 0.1 gram. The article is then submerged in a beaker of sterile saline (obtainable from the Baxter Travenol Company of Deerfield, Ill.), such that the article is totally submerged and is not bent or otherwise twisted or folded. The article is submerged for 10 minutes. The article is removed from the saline and suspended for two minutes in a vertical position to allow the saline to drain out of the article. The article is then placed body-facing surface down onto an absorbent blotter, such as the filter paper #631 available from the Filtration Science Corp., Eaton-Dikeman Division of Mount Holly Springs, Pa. A uniform 17.6 grams per square centimeter load is placed over the article to squeeze excess fluid out. The absorbent blotter is replaced every 30 seconds until the amount of fluid transferred to the absorbent blotter is less than 0.5 grams in a 30 second period. Next, the article is weighed to the nearest 0.1 gram and the dry weight of the article is subtracted. The difference in grams is the test or total capacity of the article, whichever the case may be.

[0086] The flexural resistance of the sanitary napkin is preferably in the range from about 400g to about 800 g. The flexural resistance of a sanitary napkin is meas-

ured by peak bending stiffness. Peak bending stiffness is determined by a test modeled after the ASTM D 4032-82 CIRCULAR BEND PROCEDURE, the procedure being considerably modified and performed as follows. The CIRCULAR BEND PROCEDURE is a simultaneous multi-directional deformation of a material in which one face of a specimen becomes concave and the other face becomes convex. The CIRCULAR BEND PROCEDURE gives a force value related to flexural resistance, simultaneously averaging stiffness in all directions.

[0087] The apparatus necessary for the CIRCULAR BEND PROCEDURE is a modified Circular Bend Stiffness Tester, having the following parts:

1. A smooth-polished steel plate platform which is 102.0 mm by 102.0 by 6.35 mm having an 18.75 mm diameter orifice. The lap edge of the orifice should be at a 45 degree angle to a depth of 4.75 mm;
2. A plunger having an overall length of 72.2 mm, a diameter of 6.25 mm, a ball nose having a radius of 2.97 mm and a needle-point extending 0.88 mm therefrom having a 0.33 mm base diameter and a point having a radius of less than 0.5 mm, the plunger being mounted concentric with the orifice and having equal clearance on all sides. Note that the needle-point is merely to prevent lateral movement of the test specimen during testing. Therefore, if the needle-point significantly adversely affects the test specimen (for example, punctures an inflatable structure), than the needle-point should not be used. The bottom of the plunger should be set well above the top of the orifice plate. From this position, the downward stroke of the ball nose is to the exact bottom of the plate orifice;
3. A force-measurement gauge and more specifically an Instron inverted compression load cell. The load cell has a load range of from about 0.0 to about 2000.0 g;
4. An actuator and more specifically the Instron Model No. 1122 having an inverted compression load cell. The Instron 1122 is made by the Instron Engineering Corporation, Canton, Mass.

[0088] In order to perform the procedure for this test, as explained below, five representative sanitary napkins are necessary. From one of the five napkins to be tested, some number "Y" of 37.5 mm by 37.5 mm test specimens are cut. Specimens having portions in which a cover layer is joined directly to a barrier layer or which are a laminate of a cover layer, and a barrier layer without any component of the absorbent system, should not be tested. This test is more concerned with the overall flexibility of the sanitary napkin and not merely the peripheral portions thereof and, therefore, the flexibility of the present invention is more concerned with the flexibility of the absorbent portions of the sanitary napkin.

[0089] The test specimens should not be folded or bent by the test person, and the handling of specimens must be kept to a minimum and to the edges to avoid affecting flexural-resistance properties. From the four remaining sanitary napkins, an equal number "Y" of 37.5 mm by 37.5 mm specimens, identical to the specimens cut from the first napkin, are cut. Thus, the test person should have "Y" number of sets of five identical specimens.

[0090] The procedure for the CIRCULAR BEND PROCEDURE is as follows. The specimens are conditioned by leaving them in a room that is 21 degree Celsius plus or minus 1 degree Celsius and 50% plus or minus 2.0 % relative humidity for a period of two hours. The test plate is leveled. The plunger speed is set at 50.0 cm per minute per full stroke length. A specimen is centered on the orifice platform below the plunger such that the cover layer 42 of the specimen is facing the plunger and the barrier layer 50 of the specimen is facing the platform. The indicator zero is checked and adjusted, if necessary. The plunger is actuated. Touching the specimen during the testing should be avoided. The maximum force reading to the nearest gram is recorded. The above steps are repeated until all five of the identical specimens have been tested.

CALCULATIONS

[0091] The peak bending stiffness for each specimen is the maximum force reading for that specimen. Remember that "Y" number of sets of five identical specimens were cut. Each set of five identical specimens is tested and the five values received for that set are averaged. Thus, the test person now has an average value for each of the "Y" sets tested. The flexural resistance for a sanitary napkin is the greatest of these average peak bending stiffnesses.

[0092] Applications of the product and methods of the present invention for sanitary and other health-care uses can be accomplished by any sanitary protection, incontinence, medical and absorbent methods and techniques as are presently or prospectively known to those skilled in the art. Thus, it is intended that the present application cover the modifications and variations of this invention provided that they come within the scope of the appended claims and their equivalents.

Claims

1. A sanitary absorbent article comprising:

- (A) a fluid-permeable cover layer intended for placement against a body of a wearer when the article is in use by the wearer;
- (B) a liquid-imperious barrier layer intended to face away from the body of the wearer when the article is in use by the wearer;
- (C) an absorbent structure intermediate said

cover layer and said barrier layer, said absorbent structure comprising:

- (i) a first absorbent layer, said first absorbent layer having a density of between about 0.04 g/cm³ and about 0.09 g/cm³, said first absorbent layer having superabsorbent particles incorporated therein in an amount no greater than about 15% on a weight per weight basis; and
 - (ii) a second absorbent layer having a density of between about 0.25 g/cm³ and about 0.5 g/cm³; said second absorbent layer having superabsorbent particles incorporated therein in an amount no less than about 30% on a weight per weight basis.
- 2. An absorbent article as recited in claim 1, wherein the density of said first absorbent layer is between about 0.05 g/cm³ and about 0.08 g/cm³.
- 3. An absorbent article as recited in claim 2, wherein the density of said first absorbent layer is between about 0.06 g/cm³ and about 0.07 g/cm³.
- 4. An absorbent article as recited in claim 1, wherein the density of said second absorbent layer is between about 0.35 g/cm³ and about 0.4 g/cm³.
- 5. An absorbent article as recited in claim 1, wherein the superabsorbent particles are incorporated into said first absorbent
- 6. An absorbent article as recited in claim 1, wherein the superabsorbent particles are incorporated in said second absorbent layer in an amount not less than about 45% on a weight per weight basis.
- 7. An absorbent article as recited in claim 1, wherein said second absorbent layer has a ratio of Gurley stiffness of less than about 3700.
- 8. An absorbent article as recited in claim 1, wherein said second absorbent layer has a ratio of Gurley stiffness of less than about 3200.
- 9. An absorbent article as recited in claim 1, wherein said second absorbent layer has a ratio of Gurley stiffness of less than about 3000.

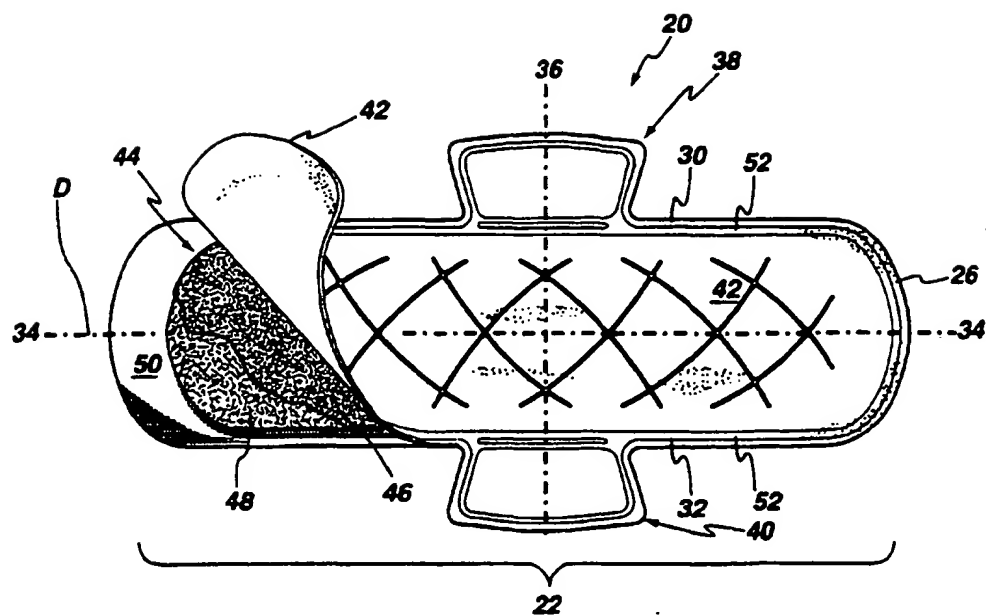


Fig.1

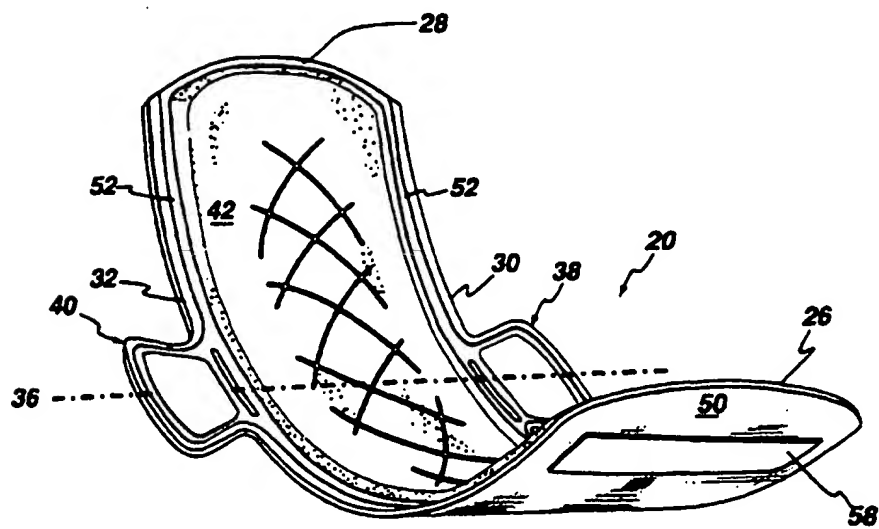


Fig.2

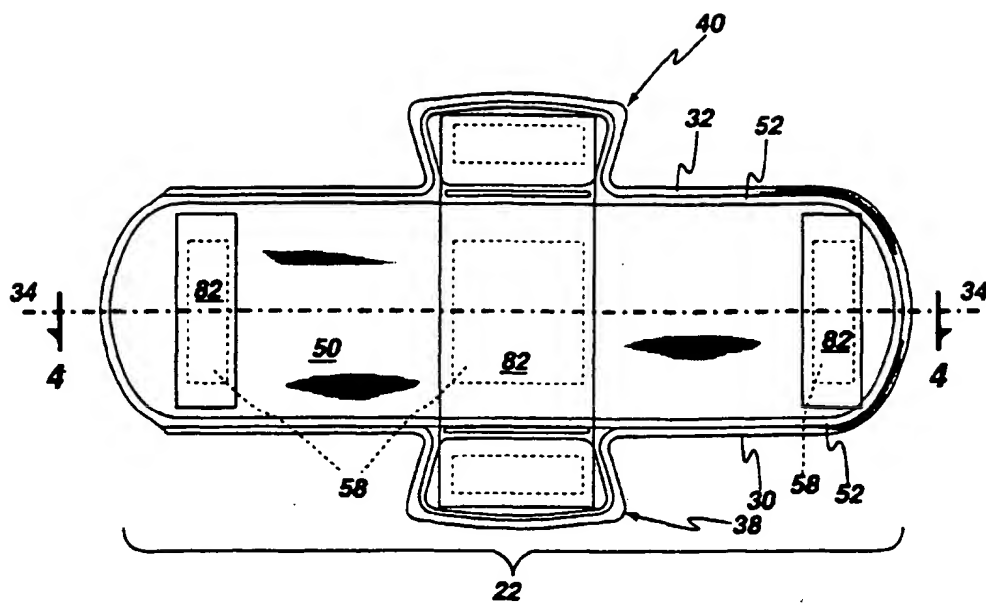


Fig.3

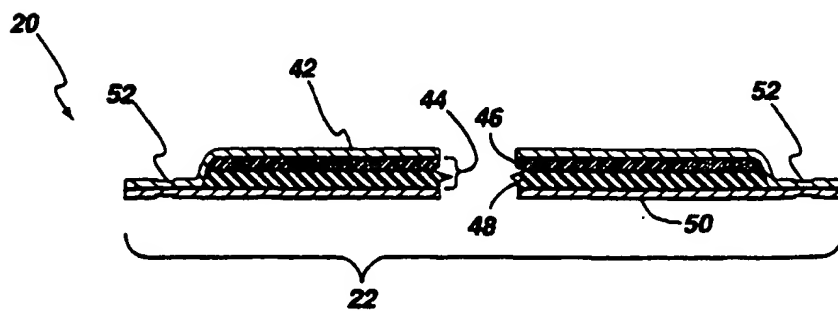


Fig.4

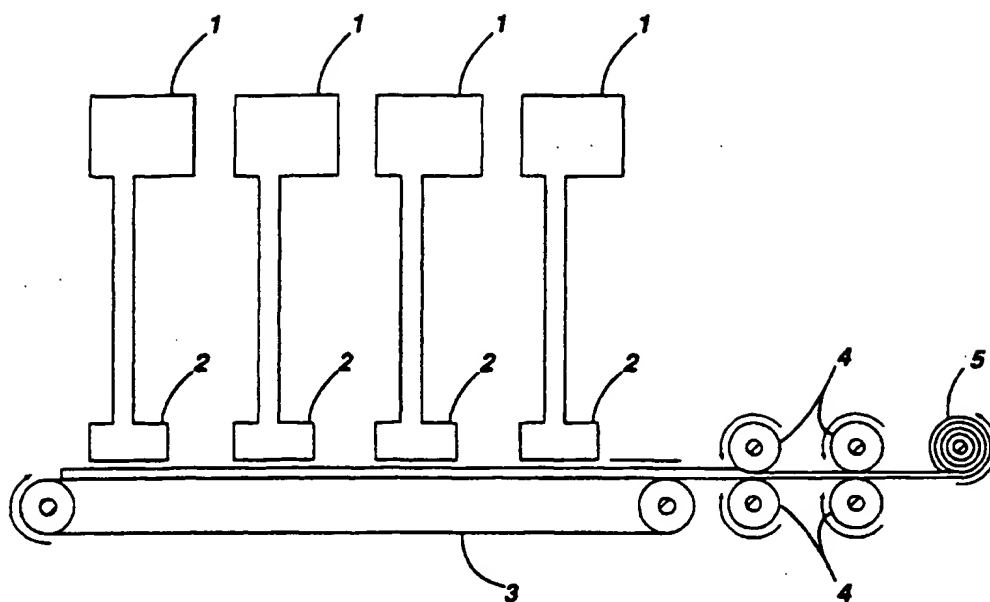


Fig. 5

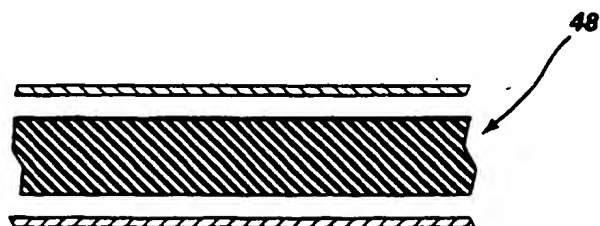


Fig. 6a

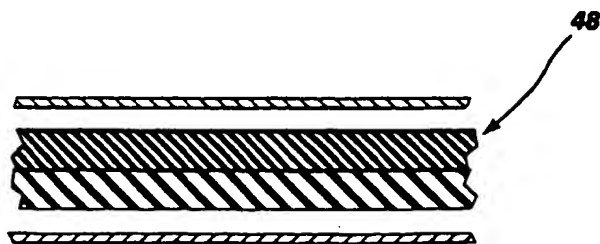


Fig. 6b